

# 1 Peng-Robinson

The Peng-Robinson equation of state is

$$P = \frac{RT}{\nu - b} - \frac{a}{\nu(\nu + b) + b(\nu - b)} \quad (1)$$

where  $\nu$  is the molar volume,  $T_c$  is the critical temperature,  $P_c$  is the critical pressure,  $\omega$  is the acentric factor, and where

$$a = a_c \left[ 1 + m \left( 1 - \sqrt{\frac{T}{T_c}} \right) \right] \quad (2)$$

$$a_c = 0.45723553 \frac{R^2 T_c^2}{P_c} \quad (3)$$

$$m = 0.37464 + 1.54226\omega - 0.26992\omega^2 \quad (4)$$

$$b = 0.077796074 \frac{RT_c}{P_c} \quad (5)$$

The cubic polynomial form of the compressibility factor is

$$Z^3 + \alpha Z^2 + \beta Z + \gamma = 0 \quad (6)$$

where

$$\alpha = B - 1 \quad (7)$$

$$\beta = A - 2B - 3B^2 \quad (8)$$

$$\gamma = B^3 + B^2 - AB \quad (9)$$

and

$$A = \frac{aP}{(RT)^2} \quad (10)$$

$$B = \frac{bP}{RT} \quad (11)$$

## 1.1 Isothermal Compressibility

Isothermal compressibility is defined as

$$\kappa = -\frac{1}{\nu} \left( \frac{\partial \nu}{\partial P} \right)_T \quad (12)$$

Taking the derivative of (6) with respect to pressure at constant temperature yields

$$3Z^2 \left( \frac{\partial Z}{\partial P} \right)_T + 2\alpha Z \left( \frac{\partial Z}{\partial P} \right)_T + Z^2 \left( \frac{\partial \alpha}{\partial P} \right)_T + \beta \left( \frac{\partial Z}{\partial P} \right)_T + Z \left( \frac{\partial \beta}{\partial P} \right)_T + \left( \frac{\partial \gamma}{\partial P} \right)_T = 0$$

which simplifies to

$$\left(\frac{\partial Z}{\partial P}\right)_T = -\frac{Z^2 \left(\frac{\partial \alpha}{\partial P}\right)_T + Z \left(\frac{\partial \beta}{\partial P}\right)_T + \left(\frac{\partial \gamma}{\partial P}\right)_T}{3Z^2 + 2\alpha Z + \beta} \quad (13)$$

the compressibility factor and molar volume are related by

$$Z = \frac{P\nu}{RT} \quad (14)$$

Therefore, molar volume can be expressed as

$$\nu = \frac{ZRT}{P} \quad (15)$$

The derivative of molar volume with respect to pressure at constant temperature is then

$$\left(\frac{\partial \nu}{\partial P}\right)_T = \frac{PRT \left(\frac{\partial Z}{\partial P}\right)_T - ZRT}{P^2}$$

which simplifies to

$$\left(\frac{\partial \nu}{\partial P}\right)_T = \nu \left[ \frac{1}{Z} \left(\frac{\partial Z}{\partial P}\right)_T - \frac{1}{P} \right] \quad (16)$$

Therefore, equations (13) and (16) can be used to calculate isothermal compressibility given the corresponding derivatives of  $\alpha$ ,  $\beta$ , and  $\gamma$ . From equations (7-9) the following derivatives are readily available

$$\left(\frac{\partial \alpha}{\partial P}\right)_T = \left(\frac{\partial B}{\partial P}\right)_T \quad (17)$$

$$\left(\frac{\partial \beta}{\partial P}\right)_T = \left(\frac{\partial A}{\partial P}\right)_T - 2(1 + 3B) \left(\frac{\partial B}{\partial P}\right)_T \quad (18)$$

$$\left(\frac{\partial \gamma}{\partial P}\right)_T = (3B^2 + 2B - A) \left(\frac{\partial B}{\partial P}\right)_T - B \left(\frac{\partial A}{\partial P}\right)_T \quad (19)$$

Finally, from equations (10) and (11) the last two required derivatives are defined as

$$\left(\frac{\partial A}{\partial P}\right)_T = \frac{a}{(RT)^2} \quad (20)$$

$$\left(\frac{\partial B}{\partial P}\right)_T = \frac{b}{RT} \quad (21)$$